Hewlett-Packard

Electronic Materials Measurement Seminar

LF and RF Parallel Plate Measurement Technique for Dielectric Substrates



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Substrate Materials Application Session

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LF and RF Parallel Plate Measurement Technique for Dielectric Substrates

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Agenda

- · Substrates Overview
- Parameters to Evaluate Dielectric Substrates
- LF Parallel Plate Technique
- Sources of Measurement Errors and Solution
- RF Parallel Plate Technique

Substrate Overview

Substrate Technologies

- Printed Wiring Board
- Thick Film
- Cofired Ceramic
- Thin Film Multilayer

Products:

- Single chip packages
- Interconnect substrates
- Multi-Chip Modules (MCMs)

Measurements:

- Capacitance
- Dielectric Constant
- · Dissipation Factor

These substrates all consist of patterned conductor layers separated by dielectric layers with conducting vias between them. The differences are in the materials used and their manufacturing processes. All of these technologies are used to produce interconnect substrates for packaged devices, for single chip packages and for multichip modules. The only difference is in the specific shape and layer count.

We will look at how capacitance and dielectric constant measurements can be used to look into these structures with an electrical eye and gain useful information about process conditions, and performance related information.

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New Product Applications are Pushing Substrate Capabilities

Analog

- RF & microwave for communication and radar
- Mixed signal converters

High Speed Digital

- Workstations, computers, uprocessors, ASICs
- Embedded controllers; automotive, consumer

Common Features:

- √ Final product performance is influenced by electrical properties of the interconnect
- √ Clock frequency can be limited by the interconnect
- $\sqrt{}$ Substrate is used to fabricate components: antennas, filters, resonators, transmission line
- √ Increasing demand for: •higher interconnect dens
 - more tightly controlled electrical performance
 - well characterized performance for simulation and modeling input
 - · shorter time to market
 - · higher quality and lower cost manufacturing processe
 - new materials with enhanced properties

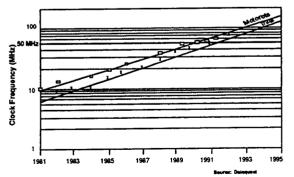
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The world of electronics is progressing at an incredible rate. This is primarily driven by the increasing expectations from the end users who expect more features, and by the IC Industry who is able to supply it. Caught in between is the packaging and interconnect industry who must supply all the infrastructure technology to integrate systems.

Substrate technologies must also advance to keep up with the requirements of the new applications. New personal communicators are driving rf and microwave products. The tidal wave of computers is driving the digital revolution.

Both types of applications have the same requirements on boards: shorter time to market, lower cost and higher quality manufacturing require more efficient R&D and more use of process monitoring. The interconnect now plays more of a role as a circuit element, and must be factored into the system level performance equation. This means dielectric constant is an important performance parameter.

New Market Directions: Higher Clock Frequencies



Applications moving toward higher clock frequencies:

- √ Lower dielectric constant is needed
- √ Controlled impedance interconnects are needed
- √ Capacitance per length is spec'd

RF and microwave applications have always been operating at high bandwidths in the hundreds of megahertz range. In the last few years, digital applications have begun to catch up. Off the shelf digital products have clock frequencies over 50 MHz, and analog bandwidths in the 250 MHz range.

This trend is on an exponentially increasing track. In a few years, the bandwidth of signals in digital applications will be just as high as for rf and microwave applications. In this regime, electrical aspects of the interconnect substrates, such as time of flight and characteristic impedance are important terms in both analog and digital applications.

Impact on Substrate Technologies

State of the art is continually being pushed:

- New materials are being developed
- New processes are being developed

R&D: shorter development cycle times

√ More efficient evaluation of materials and processes needed

Manufacturing: lower cost, higher quality

- √ Tighter process control and SPC a must
- √ More use of incoming and outgoing QC testing
- √ 100% open/short testing on tighter than 100 mil centers common

Users want more performance related information:

Trace capacitance Dielectric Constant

Full SPICE Deck, transmission line parameters

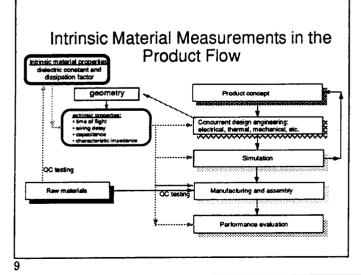
This advance in IC technology and product features means substrates must continually advance as well. The three big issues are higher performance, faster time to market and lower cost, higher quality manufacturing.

In addition, the end users of the substrates, who are responsible for integrating them into products need more information about their electrical performance so that accurate simulations can be performed, and to verify that the substrates meet the electrical specs.

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There are two types of properties: intrinsic and extrinsic. Dielectric constant and dissipation factor are intrinsic properties in that these are properties of the material independent of the sample size of the material. As a fundamental property of the material, these two parameters act as a window into the state of the materials. They can be used as quality control terms to evaluate the reproducibility of the material and its state during the manufacturing processing.

All of the performance related properties are extrinsic in that these properties depend also on the geometry.

In the product evolution flow, the geometry and material properties are important ingredients to simulations of the system performance. These performance related properties are often monitored along the manufacturing path to verify that the final product has the specified properties.

How the intrinsic material properties are factored into the extrinsic performance properties is explored in the following slides.

Permittivity

Describes the interaction of a material with an electric field

$$\mathsf{K} = \varepsilon_{\mathsf{r}} = \frac{\varepsilon''}{\varepsilon_{\mathsf{o}}}$$

$$\mathsf{K}' = \varepsilon'_{\mathsf{r}} = \frac{\varepsilon''}{\varepsilon_{\mathsf{o}}} = \varepsilon'_{\mathsf{r}} - \mathsf{j} \ \varepsilon''_{\mathsf{r}} = \left(\frac{\varepsilon'}{\varepsilon_{\mathsf{o}}}\right) - \mathsf{j} \ \left(\frac{\varepsilon''}{\varepsilon_{\mathsf{o}}}\right)$$
(storage) (loss)

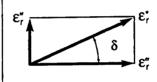
K = dielectric constant

 \mathcal{E}_r' = relative permittivity

En = permittivity of free space

 $=\frac{1}{36} \times 10^{-9}$ Farad/meter

Loss Tangent



$$\tan \delta = \frac{\mathcal{E}_r''}{\mathcal{E}_r'} = \frac{\mathcal{E}''}{\mathcal{E}'} = \frac{\mathcal{K}''}{\mathcal{K}'}$$

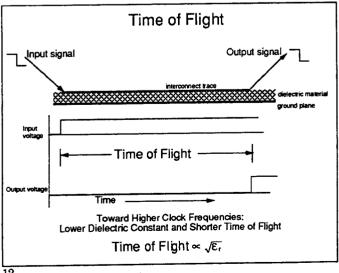
 $tan \delta = D$ (Dissipation Factor)

 $=\frac{1}{C}$ (Inverse Quality Factor)

cc Energy Lost per Cycle Energy Stored per Cycle

Permittivity (£) describes the interaction of a material with an electrical field. Dielectric constant (K) is equivalent to relative permittivity (\mathcal{E}_r) or the absolute permittivity (\mathcal{E}) of free space (\mathcal{E}_0). The real part of permittivity (\mathcal{E}'_7) is a measure of how much energy from an external electric field is stored in a material. The imaginary part of permittivity (\mathcal{E}_r^r) is called the loss factor and is a measure of how dissipative or lossy a material is to an external electric field.

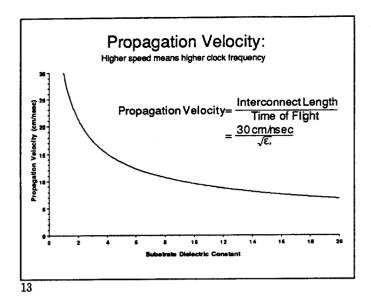
When complex permittivity is drawn as a simple vector diagram, the real and imaginary components are 90 degrees out of phase. The vector sum forms an angle δ with the real axis (\mathcal{E}'_{r}). The relative "lossiness" of a material is the ratio of the energy lost to the energy stored.



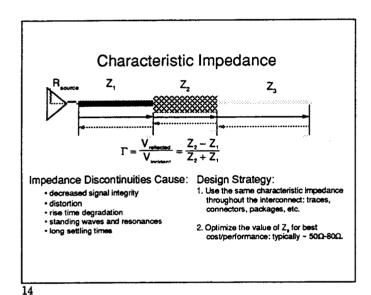
In digital applications, higher clock frequency means shorter clock periods. The time it takes for a signal to propagate from one chip to the next on the board can limit how short a period is possible. To get shorter periods, a shorter time of flight is required.

The time of flight for a signal how long it takes to get from the output on one chip to the input of another. It depends on the length of the interconnect, and the dielectric constant of the material surrounding the signal trace.

Merely by changing the dielectric constant of the insulation, the time of flight will change. The lower the dielectric constant, the shorter the time of flight.



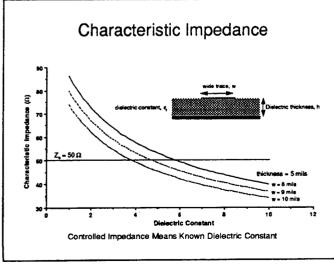
A related term is the speed of a signal, or propagation velocity. This is directly related to the sqrt of the dielectric constant. The faster the signals move in the substrate, the better chance there will be for a higher clock frequency. This is why it is so important to move toward lower dielectric constant materials.



Characteristic impedance is perhaps the most commonly used term in high speed circuits, and the most confused term. It is a property of the interconnect and relates how the voltage and current signals interact as its moves down the interconnect trace. The key feature is that when the characteristic impedance changes, either by a geometry change or material change, some of the signal will be reflected.

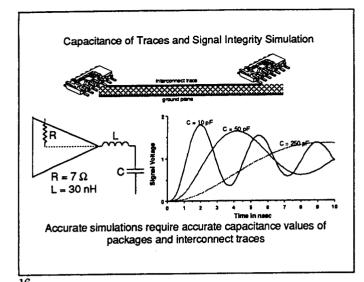
At each interface, there will be a series of reflections. These will result in a decrease in overall signal integrity.

The way to get around this problem is to use controlled impedance interconnects. Every section of trace, connector and package should have the same characteristic impedance. Most systems use a value of 50Ω to 80Ω . The precise value is a trade off between manufacturability, cost, noise sensitivity and power dissipation.



Characteristic impedance depends on the intrinsic material property of dielectric constant, and the cross sectional geometry. For the specific case of microstrip, the line width and dielectric thickness influence the characteristic impedance.

In the particular case analyzed here, the dielectric thickness is 5 mils. For a dielectric constant of 4.9 and a target of $50\Omega,$ a 9 mil wide trace will do it. If the line width should vary by ± 1 mil, the characteristic impedance would vary by about $\pm 10\%.$ If the dielectric constant were to vary by $\pm 10\%,$ the characteristic impedance would vary by about $\pm 5\%.$ It is not as sensitive to characteristic impedance as the line width.



The last example of a performance property is the capacitance of the interconnect. It is one of a number of parasitic properties that must be used in simulations.

In this example, the wave form seen at the end of an interconnect is simulated. It depends on the chip driver features, the package the chip is in, and the capacitance of the interconnect. If the interconnect capacitance changes, the simulated waveform will change.

End Users are Demanding More Characterization Information

- $\sqrt{\rm Dielectric}$ constant, propagation velocity, wiring delay $\sqrt{\rm Capacitance}$ per trace
- Resistance per trace
- · Inductance per trace
- · Characteristic impedance of traces
- Cross talk coupling coefficients

In high speed applications, the substrate electrical properties influence circuit performance. This means that in order to simulate the product performance, the interconnect electrical circuit parameters are required. All high speed system designers are demanding more of this type of information.

The terms that will be measured in this seminar are related to dielectric constant and capacitance. Other parameters such as resistance, inductance, characteristic impedance and cross talk can also be measured with similar techniques, but not described here.

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Dielectric Constant and Dissipation Factor: Intrinsic Material Properties $\epsilon_r = \frac{\epsilon'}{\epsilon_0} \text{ ~energy storage } \qquad \tan(\delta) = \frac{\epsilon''}{\epsilon'} \text{ ~energy loss } \\ \epsilon_0 = 8.85 \text{x} 10^{-14} \text{ F/m} \\ = 0.088 \text{ pF/cm} \\ = 0.225 \text{ pF/inch} \\ \frac{\epsilon}{10^3 \text{ loss}} = \frac{10^3 \text{ loss}}{10^4 \text{ loss}} = \frac{10^{12} \text{ loss}}{10^{13} \text{ loss}} = \frac{10^{14} \text{ loss}}{10^{14} \text{ loss}}$

The dielectric constant of a material is actually a complex number. The real part of it is often what we call the dielectric constant. It relates to the energy storage in electric fields by the material. We often normalize it to the permittivity of free space so that we deal with small, dimensionless numbers. Often we refer to the "relative" dielectric constant.

The imaginary component relates to the energy dissipated in the material by the electric fields. The ratio of the imaginary to the real is what we refer to as the dissipation factor or the tangent of the loss angle.

Neither of these terms are actually constant. They both vary with the frequency of the electric field. At frequencies below 1 GHz, typical for most electronic applications, these terms are generally flat with frequency, and drop off at higher frequencies.

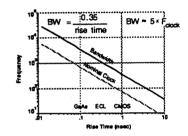
With this frequency dependence, it is important to address the question, at what frequency should the dielectric constant measurements be performed?

Material and performance related measurements should always be performed up to at least the bandwidth of the application. In analog applications, the bandwidth is often the clear.

In digital applications, the bandwidth can be found from either the rise time or the clock frequency, depending on which is known. With a clock frequency of 50 MHz, the bandwidth is about 250 MHz.

For all new materials that have no prior data base, measurements should be made up to the full bandwidth. If this is over about 40 MHz, it will require the use of a network analyzer, and is more complicated than an impedance analyzer. However, most interconnect materials have a dielectric constant that is relatively flat with frequency, so that low frequency measurements can be used to relate to high frequency performance.

Application Bandwidth, Measurement Range and Material Properties

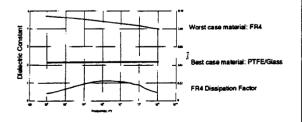


- Typical high speed digital clock frequency ~ 50 MHz; BW = 250 MHz
- All new materials should be measured up to full bandwidth of application
- Network Analyzer required for frequencies > 40 MHz
- · Most interconnect materials have flat dielectric constant with frequency

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Frequency Variation of Interconnect Materials (Must be evaluated on a case by case basis)



Source: Mumby and Schwarzkopf, AT&T, e. 500 of Electronics Materials Handbook, ASM, 1989 Here is an example of the actual frequency variation in dielectric constant for the most varying material, FR4, and the most constant material, Teflon.

Even as worst case, FR4 varies only about 10% from 100 kHz to 1 GHz. For some applications, this can be considered flat. All other interconnect dielectrics vary much less than this.

This means that a measurement done at 1 MHz, for example, has relevance at 100 MHz.

However, until it is established that the dielectric constant is constant over frequency, high frequency measurements are still needed at some point for all new materials.

The frequency variation must be analyzed for all materials on a case by case basis.

Why Impedance Analyzer/LCR Meter** and Parallel Plate Technique

- 1. Simple sample preparation for thin, flat structures
- 2. Simple fixturing
- 3. Simple instrument
- 4. Low cost
- 5. Adequate for most materials that are constant over frequency
- 6. IDEAL for fast, routine measurements

* Impedance analyzers use a synthesized frequency source and can sweep in frequency I CB meters use fixed frequency values. If low frequency measurements are acceptable, an impedance analyzer can be used. The chief value of the impedance analyzer is its ease of use and low cost compared to a network analyzer.

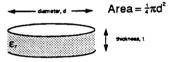
Samples are typically in sheet form and can be measured using a parallel plate technique, often with no special preparation at all.

This combination is ideal for fast, routine measurements, and may open up a few applications that did not exist before because it was too complicated.

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Parallel Plate Technique

Measuring Dielectric Constant from Capacitance and Geometry



Ideal parallel plate capacitor.

$$C = \varepsilon_0 \varepsilon_r \frac{\text{Area}}{t} \qquad \varepsilon_r = \frac{Ct}{\varepsilon_0 \text{Area}}$$

 $\varepsilon_0 = 8.85 \times 10^{-14} \text{ F/m}$ = 0.088 pF/cm

= 0.225 pF/inch

Non-ideal effects:

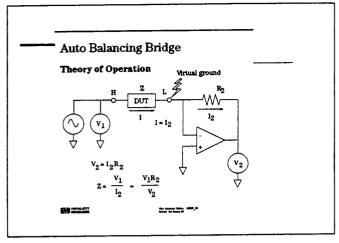
- stray parasitics with the cabling
- \bullet fringe fields around the edges (for less than 3%, need d >100 t)

The basis of measuring dielectric constant is from measuring the capacitance of a pancake sample of the material made with electrodes on opposite sides. The capacitance is related exactly to the geometry and dielectric constant when the sample is in this parallel plate configuration.

From the measured capacitance, surface area of electrodes and plate separation, the dielectric constant can be calculated. The measured dissipation factor is the actual material dissipation factor.

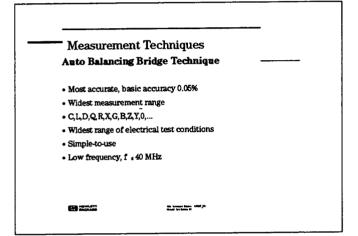
However, there are two artifacts which make this simplified analysis too simple. One is stray parasitics from the cabling and the other is fringe fields. These are compensated for with the four terminal impedance analyzer and the HP 16451B fixture.

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For low frequency, the four terminal or auto balancing bridge technique is very effective for measuring dielectric substrates using the parallel plate fixture. The auto balancing bridge can be conceptionilized as an optional amplifier: V=I*R.

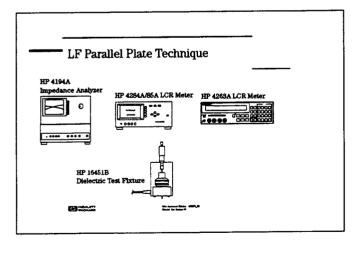
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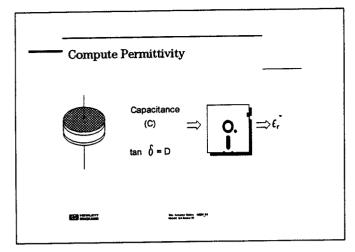
The auto balancing bridge technique is by far the best technique for measurements below 40 MHz. It provides the most accurate measurements possible and the widest impedance measurement range. Both of these are critical for accurate material analysis.

A wide range of AC and DC stimuli can be applied to the material. In addition, this low frequency technique is the simplest measurement technique to use.

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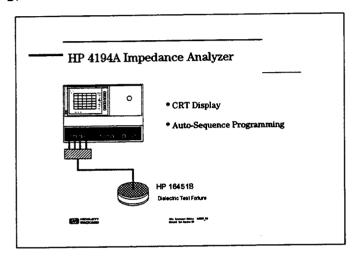


Hewlett-Packard offers several LCR meters and Impedance Analyzers plus the HP 16451B Dielectric Test Fixture for LF Parallel Plate solutions.



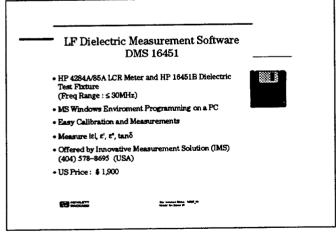
The parallel plate method involves sandwiching a thin sheet of material between two electrodes to form a capacitor. An LCR meter or impedance analyzer is used to measure the loaded fixture. ϵ_r is computed from the measurement of capacitance and ϵ_r is computed from the measurement of dissipation factor (D).

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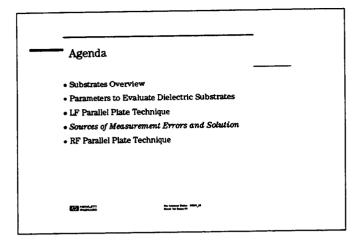


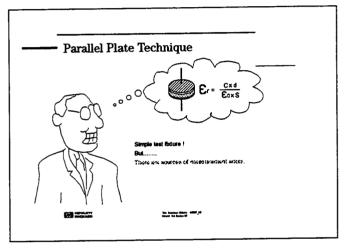
The HP 4194A Impedance Analyzer can display the capacitance and dissipation factor frequency response from 100 Hz to 40 MHz on its color CRT. In addition, the HP 4194A can compute and display permittivity vs frequency using the built-in programming capability called "Auto-Sequence Programming."

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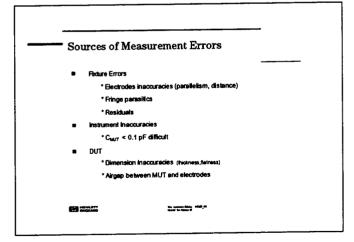


Innovative Measurement Solution (IMS) has just introduced the DMS 16451 (LF Dielectric Measurement Software). It works on a PC MS windows environment, and it's applicable for the HP 4284A/HP 4285A with the HP 16451B. It allows you to perform the easy calibration and auto calculation for permittivity, and loss tangent.

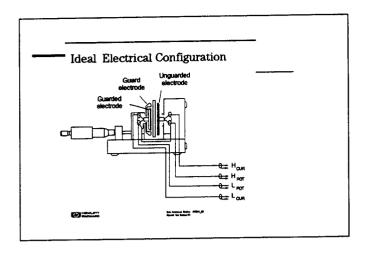




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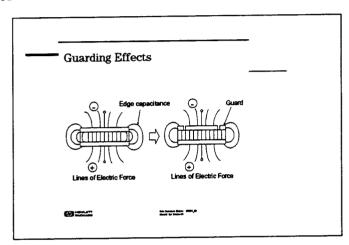


To measure dielectric constant accurately, we have to consider the sources of measurement errors. We will learn how we can minimize these errors in the following slides.



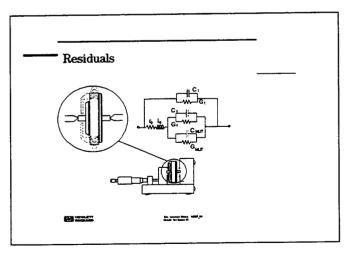
This is the ideal electrical configuration of dielectric test fixture. It has three electrodes; a unguarded electrode which connects to high terminal, guarded electrode which connects to low terminal, and guard electrode which connects to guard terminal.

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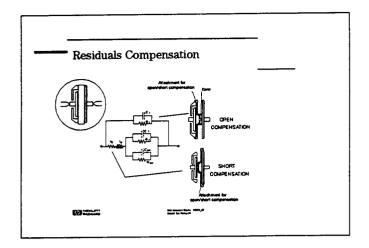


Guard electrode eliminates the error comes fringe parasitics. When we don't have a guard electrode, the current that flows through the stray capacitance causes measurement error. But when we guard electrode, it eliminates the current flowing perpendicular to the material. The current flows to the guard electrode eliminating measurement error because the current is not measured.

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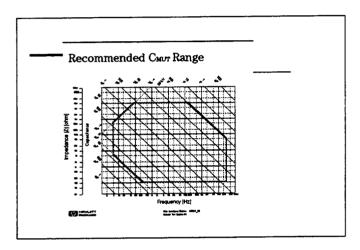


All test fixtures have residuals such as residual impedance(r0, I0) and stray admittance(Ct, Gt). This slide shows where residuals exist on the dielectric test fixture. Note that Cmut and Gmut is what we want to measure.



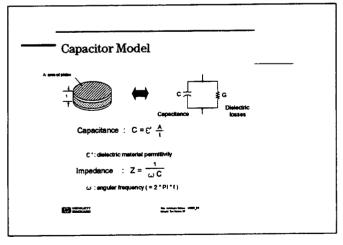
To remove errors from residuals, we have to perform open/short compensation. Open compensation eliminates the error from stray admittance. Short compensation eliminates the error from residual impedance. An attachment for open/short compensation are necessary for accurate compensation.

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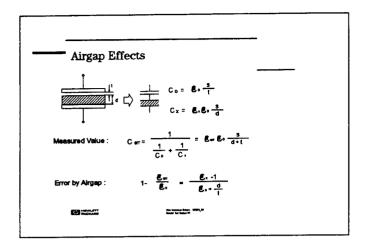


It is important to select the size of the material such that its capacitance value is within range of the measurement equipment. For example it is difficult to measure 0.1pF or smaller because of instrument inaccuracies. Since the capacitance value is decided by the size of sample material, we have to select the sample size in order to have the sample material impedance enter appropriate impedance range in the slide.

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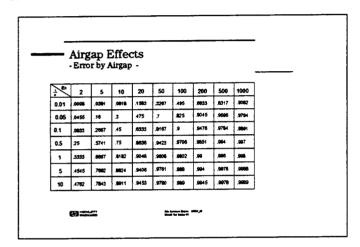


The capacitance of the material is calculated by the dielectric constant and sample size. And impedance of material is calculated by the capacitance of material and measurement frequency. When we measure the material at a certain frequency, we can estimate the measured impedance value by assuming the dielectric constant value of material. It is better that the impedance value is medium range(1kohm - 1Mohm), which LCR Meter and Impedance Analyzers can measure accurately.



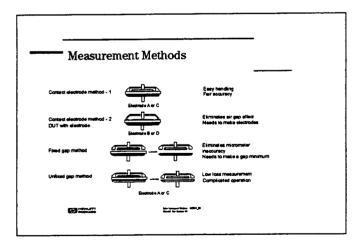
Airgap between the material and electrodes causes measurement error. When there is airgap thickness between material and electrode, the LCR meter and impedance analyzer measures the sum of capacitances by the dielectric material (MUT) and air. The airgap error calculation is shown in the slide.

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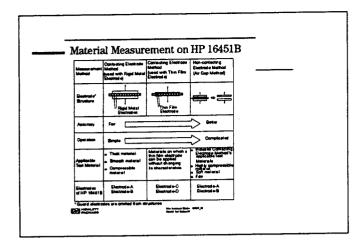


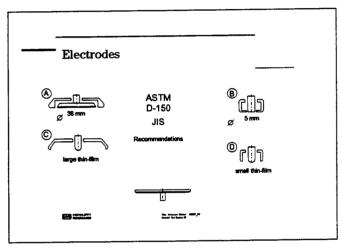
The table shows how much error there is for a given airgap between the material and electrode. Note that the airgap is more serious when we measure high dielectric constant materials.

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There are a couple of measurement methods available by the parallel plate technique. Each technique has an advantage and disadvantage. Please refer to the HP Application Note 380-1, "Dielectric constant measurement of solid materialsusing the HP16451B test fixture".





There are three applicable measurement methods for the HP 16451B.

There is the Contacting Electrode method(rigid metal electrode), the Contacting Electrode method(with thin film electrode) and the Non-Contacting Electrode method. These three methods are different in operation and measurement accuracy. The contacting electrode method is the simplest method of all while the contacting method with the thin film electrode is effective for thin materials.

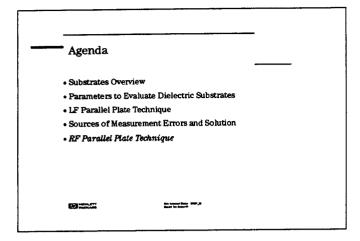
The non-contacting method is the most accurate method of all. A suitable measurement method and electrode for your test material can be selected to measure any material accurately.

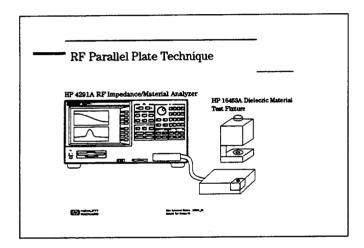
To measure many types of material shape, we need many types of electrodes. For exapmpe, Electrode-A and Electrode-B are the electrodes for materials which don't have electrode on the surface. Electrode-C and Electrode-D are the electrodes for material which have thin film electrodes on the surface.

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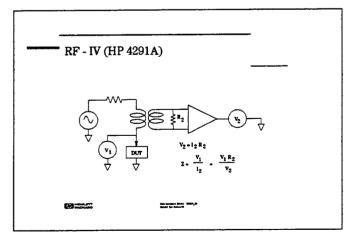
Airgap method				
* Airgep between N				
Dimension med				
* Dimension inaccu	racios ((thickness, Eatnes	13)	
* C∞ur < 0.1 pF of fi	cuit 🖒 Sam	pie size consider	8 DCM	
Instrument Inaccuracies			nton	
*Residuals 🖒 C		mpersatori		
* Fringe parasitics				
Adjustment wi			nt	
Pixture Errors * Electrodes inaccu	-			
and Solution Su	mmary			
Sources of M		nent Error	•	

We must follow these procedures to minimize measurement errors.

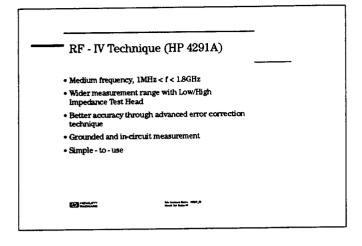




The RF parallel plate technique uses the new HP 4291A Impedance/Material Analyzer and the HP 16453A Dielectric Material Test Fixture. The HP 4291A with opt 002 will automatically calculate and display permittivity and loss tangent vs frequency. (You don't need an external computer!) This solution uses the RF-IV measurement technique.



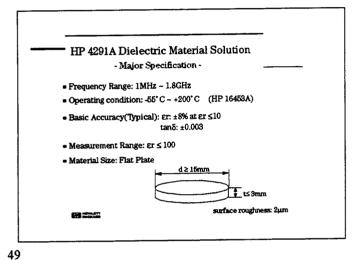
The RF - IV technique measures two voltages; V1 is measured across the DUT and V2 across a low-loss transformer. This technique is bandwidth-limited because of pick-up transformer, however the HP 4291A expands frequency range up to 1.8GHz by using a wide bandwidth balun transformer.



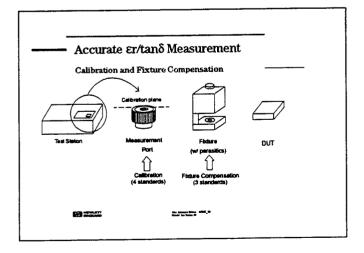
The RF - IV technique provides very good mid-frequency range performance, extending up to 1.8GHz.

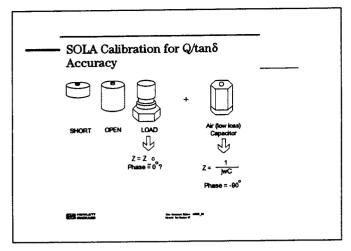
This technique has a very good impedance measurement range with quite good accuracy, since the HP 4291A uses advanced error correction technique like the Open/Short/Load/Air Capacitor Calibration and Open/Short/Load Compensation.

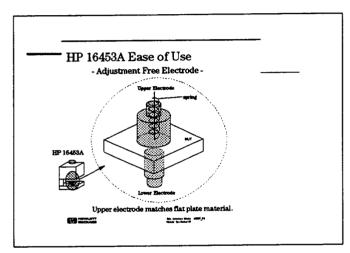
48



The new HP 16453A uses the parallel plate method, and its upper electrode has a spring inside that pushes the material to fit in the fixture easily. You don't need to adjust the flatness of the electrode like an HP 16451B. (LF Parallel Plate fixture).

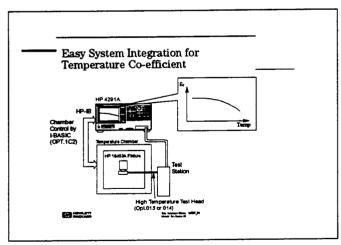






The HP 4291A accurately measures relative permittivity and loss tangent up to 1.8 GHz with the operating codition from -55 degree C to 200 degree C. The required material size is less than 3 mm in thickness.

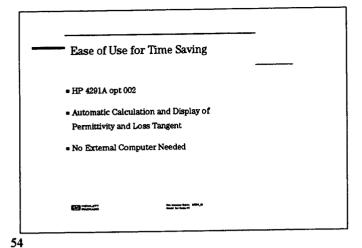
52



The HP 4291A provides the following features and options to simplify evaluating temperature characteristics.

- 1. 1.8 error-free cables
- 2. High temperature test head option
- 3. Built-in HP-IB
- 4. Optional I-Basic
- 5. Application Program (I-BASIC) Available

Tabai Espec Corporation offers a temperature chamber (SU-240-Y) compatible with the HP 4291A.



The HP 4291A with Option 002 will automatically calculate and display the relative permittivity values eleminating the need to calculate the parameters using an external computer.

Prequency Range

OF Prequency swept measurements

OHZ-15MHz

OHZ-15MHz

OHZ-30MHz

OHZ-3

This slide shows the HP selection of LF and RF Parallel Plate solutions for dielectric substrates. You should pick the solution that meets your swept or spot frequency needs.

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